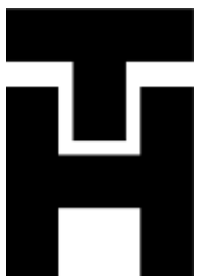


DRAINAGE STUDY
PHASE 2 – ALTERNATIVE IMPROVEMENTS
CRYSTAL LAKE
ALTERNATIVE 4C IMPROVEMENTS

FOR:
LAKWOOD – PIRATELAND SWASH
HORRY COUNTY, SC

APPENDIX A

J-23453.0001



Prepared by:

THOMAS & HUTTON

REPORT OF GEOTECHNICAL EXPLORATION

Crystal Lake Modifications

Horry County, South Carolina
S&ME Project No. 1633-13-127

Prepared For:

Thomas & Hutton
Post Office Box 1522
Mount Pleasant, South Carolina 29465

Prepared By:



1330 Highway 501 Business
Conway, South Carolina 29526

May 16, 2013



May 16, 2013

Thomas & Hutton
Post Office Box 1522
Mount Pleasant, South Carolina 29465

Attention: Mr. Rick Karkowski, P.E.

Reference: **Report for Geotechnical Exploration**
Crystal Lake Modifications
Horry County, South Carolina
S&ME Project No. 1633-13-127

Dear Mr. Karkowski:

S&ME, Inc. is pleased to submit this report of soil test boring results for the referenced site. The exploration was performed to evaluate subsurface conditions surrounding Crystal Lake, and was performed in general accordance with S&ME Proposal number 1633-0357-12.r1, dated January 4, 2013, and authorized on April 15, 2013 via email correspondence. This report presents a brief discussion of our understanding of the project and the results of our exploration.

PROJECT INFORMATION AND SITE DESCRIPTION

Crystal Lake is an existing lake of approximately 39.46 acres in area, located within a residential area of Horry County, near Surfside Beach, South Carolina. We understand that modifications to the lake and related drainage features are under consideration by Horry County, in order to improve stormwater drainage in the local area. The modifications may include dredging and/or excavation of the existing lake and altering the lake normal water level (NWL) by design and construction of replacement downstream control structures.

Although design is in the preliminary stages at this time, we understand that the existing lake NWL will likely be lowered about 4.4 feet, and that the post-construction lake bottom will be about 6 feet below the new NWL. It is anticipated that dredging depths of up to about 10 feet may be required to remove existing materials beneath the lake and achieve design contours.

According to the available information, Crystal Lake was created after the site was utilized as a local borrow source for residential development. It is presumed that borrow



excavation did not extend to depths beneath the existing lake bottom surface, such that materials underlying the lake are relatively undisturbed Coastal Plain deposits, rather than fill materials placed back into an over excavated borrow area. The lake was observed to be relatively shallow, with several area grassy area sandbars observed and water depths of about 6 feet or less.

A site vicinity plan of the project site is provided in the Appendix as Figure 1.

EXPLORATION PROGRAM

Four soil test borings were conducted at the approximate locations shown on the Test Location Sketch in the Appendix as Figure 2. The borings were performed using a trailer drill rig. Mud rotary techniques were used to advance the boring to the termination depth of 20 feet for B-1 and B-2 and 30 feet for B-3 and B-4.

Standard Penetration Tests (SPT) were performed in the borings using an automatic hammer, at 2.5-foot intervals in the top 10 feet, then at 5-foot intervals thereafter, in general accordance with ASTM D 1586, to provide an index for estimating strength parameters and relative consistency of subsurface soils. Subsurface water measurements were unable to be accurately measured upon completion of drilling due to use of drilling fluids. However water level measurements were obtained approximately 24 hours after the completion of drilling of the test borings. Split-spoon samples routinely obtained from the standard penetration tests were transported to our laboratory and visually classified according to the textural nomenclature of the Unified Soil Classification System (ASTM D 2488).

SUBSURFACE CONDITIONS

Detailed descriptions and stratifications are provided on the Boring Logs located in the Appendix. A brief summary of the conditions encountered at our boring locations for each proposed sign location is provided below.

Surface Conditions

At boring locations B-1, B-2, and B-4 sparse grass was encountered at the surface with approximately 3 inches of topsoil. No topsoil was encountered at boring location B-3.

Soil Stratification

Starting from the surface at boring B-3 and underlying the 3 inches of topsoil at the remaining borings we generally encountered poorly graded sand (SP), and silty sands (SP-SM) until termination of borings. These soils consisted of mostly fine to medium sands with few to trace of low to medium plasticity fines. These soils were typically tan, brown, and gray in color, and were moist to saturated. The SPT N-value of these soils ranged from 3 to 17 blows per foot (bpf) indicating a very loose to medium dense relative density. These soils are suitable for reuse as construction materials after the soils are excavated and allowed to dry to within 3 percent of their optimum moisture contents.

In boring B-3 an elastic silt (ML) was encountered from depths 8.5 feet to 13 feet. This soil consisted of mainly medium to high plasticity fines with few fine sands. It was gray in color and saturated. The SPT N-value for this material was 1 (bpf) indicating a very soft consistency.

Laboratory testing was conducted on one sample from each boring. An overview of the sample data is provided in Table 1 below.

Table 1 – Laboratory Testing

Boring	Depth ft.	Classification	Natural Moisture	Fines Content	Liquid Limit	Plastic Limit	Plastic Index
B-1	6.0 – 7.5	SP-SM	42.9%	5.5%	N/A	N/A	NP
B-2	13.5 – 15.0	SP	22.3%	1.7%	N/A	N/A	NP
B-3	8.5 – 10.0	ML	87.9%	72.4%	47	32	15
B-4	13.0 – 15.0	SP	31.9%	1.8%	N/A	N/A	NP

Detailed laboratory results are provided for your review in the Appendix.

Subsurface Water

An overview of the subsurface water conditions encountered at each of the proposed sign locations is provided in Table 2 below.

Table 2 – Subsurface Water Conditions

Boring	Water Depth Below Surface in Feet
	After 24 hours
B-1	0
B-2	0
B-3	3.5
B-4	10

Subsurface water levels may fluctuate seasonally at the site, being influenced by rainfall variation and other factors. Site construction activities can also influence water elevations.

LIMITATIONS OF THIS REPORT

This report has been prepared in accordance with generally accepted engineering practice for specific application to this project. Any wetland, environmental, or contaminant assessment efforts are beyond the scope of this geotechnical exploration and therefore, those issues are not addressed in this geotechnical exploration report. No other warranty, expressed or implied, is made.


Analysis submitted in this report is based, in part, upon the data obtained from the geotechnical exploration. The nature and extent of variations between and outside of the boring made may not become evident until excavation begins.

CLOSURE

S&ME, Inc. appreciates the opportunity to have provided our geotechnical services on this project. If you have any questions concerning this report, please do not hesitate to contact us at (843) 347-7800.

Respectfully submitted,
S&ME, Inc.


Joshua D. Jordan E.I.T.
Staff Professional


Christopher J. Brown, P.E.
Engineering Department Manager

APPENDIX

SITE VICINITY PLAN

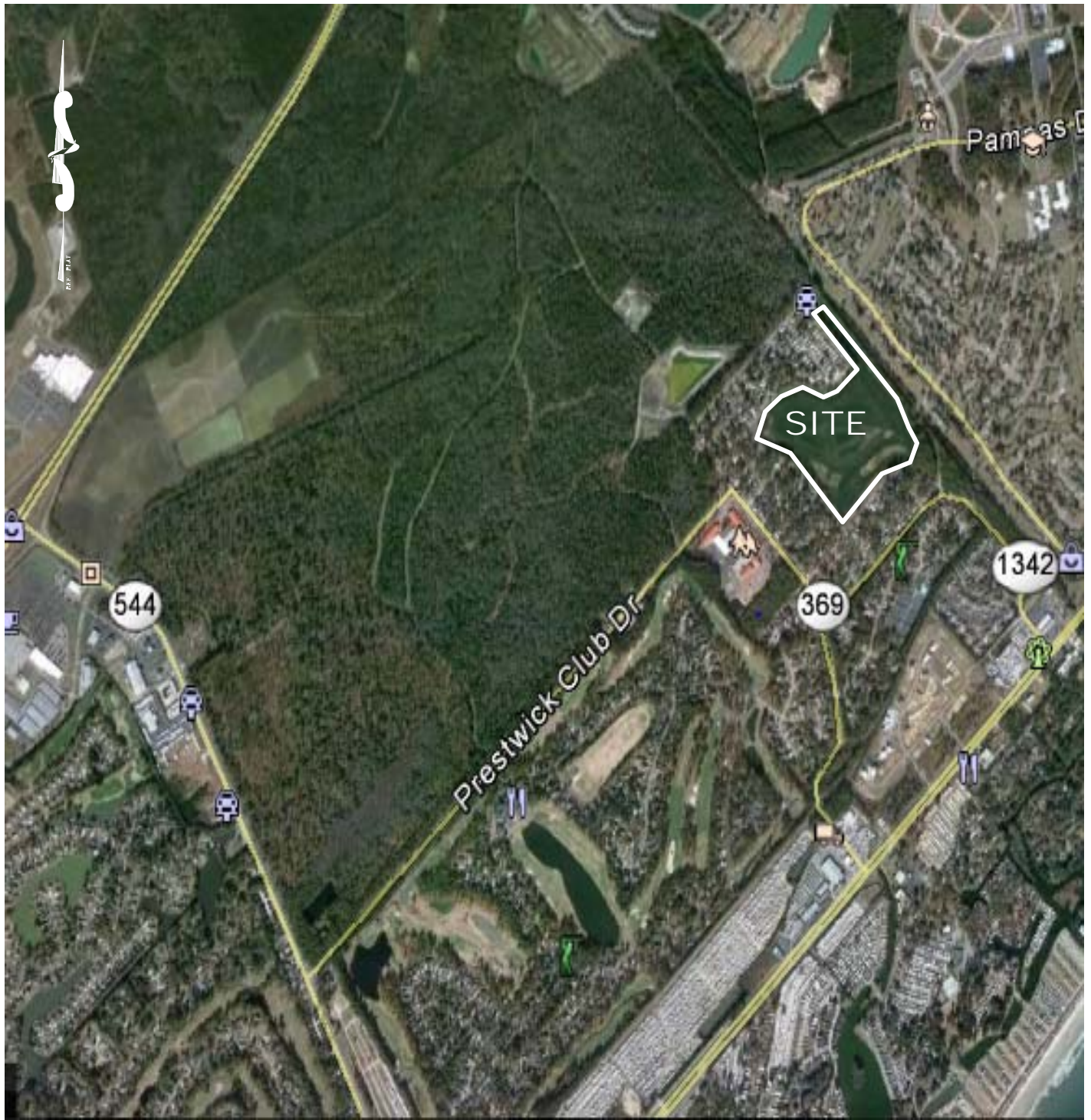
TEST LOCATION SKETCH

SUMMARY OF EXPLORATION PROCEDURES

SOIL CLASSIFICATION CHART

SOIL TEST BORING LOGS

LABORATORY TEST RESULTS



SCALE:	NTS
SOURCE:	Google
DRAWN BY:	CJB
DATE:	April 29, 2013



Site Vicinity Map
 Crystal Lakes Mobile Home Park
 Myrtle Beach, South Carolina

JOB NO. 1633-13-127

FIGURE NO

1



B-1 – 20 foot boring

B-2 – 20 foot boring

B-3 – 30 foot boring

B-4 – 30 foot boring



Approximate Boring Location



SCALE:	NTS
SOURCE:	Google
DRAWN BY:	CJB
DATE:	April 29, 2013



Test Location Sketch
 Crystal Lakes Mobile Home Village
 Myrtle Beach, South Carolina

JOB NO. 1633-13-127

FIGURE NO

2

SUMMARY OF EXPLORATION PROCEDURES

The American Society for Testing and Materials (ASTM) publishes standard methods to explore soil, rock and ground water conditions in Practice D-420-98, “*Standard Guide to Site Characterization for Engineering Design and Construction Purposes.*” The boring and sampling plan must consider the geologic or topographic setting. It must consider the proposed construction. It must also allow for the background, training, and experience of the geotechnical engineer. While the scope and extent of the exploration may vary with the objectives of the client, each exploration includes the following key tasks:

- Reconnaissance of the Project Area
- Preparation of Exploration Plan
- Layout and Access to Field Sampling Locations
- Field Sampling and Testing of Earth Materials
- Laboratory Evaluation of Recovered Field Samples
- Evaluation of Subsurface Conditions

The standard methods do not apply to all conditions or to every site. Nor do they replace education and experience, which together make up engineering judgment. Finally, ASTM D 420 does not apply to environmental investigations.

RECONNAISSANCE OF THE PROJECT AREA

Where practical, we reviewed available topographic maps, county soil surveys, reports of nearby investigations and aerial photographs when preparing the boring and sampling plan. Then we walked over the site to note land use, topography, ground cover, and surface drainage. We observed general access to proposed sampling points and noted any existing structures.

Checks for Hazardous Conditions - State law requires that we notify the Palmetto Utility Protection Service (PUPS) before we drill or excavate at any site. PUPS is operated by the major water, sewer, electrical, telephone, CATV, and natural gas suppliers of South Carolina. PUPS forwarded our location request to the participating utilities. Location crews then marked buried lines with colored flags within 72 hours. They did not mark utility lines beyond junction boxes or meters. We checked proposed sampling points for conflicts with marked utilities, overhead power lines, tree limbs, or man-made structures during the site walkover.

BORINGS AND SAMPLING

Soil Test Boring with Rotary Wash

Soil sampling and penetration testing were performed in general accordance with ASTM D1586, “*Standard Test Method for Penetration Test and Split Barrel Sampling of Soils.*” A rotary drilling process was used to advance the hole and a heavy drilling fluid was circulated in the bore holes to stabilize the sides and flush the cuttings. At regular intervals, drilling tools were removed and soil samples were obtained with a standard 1.4 inch I. D., two-inch O. D., split barrel sampler. The sampler was first seated six inches to

penetrate any loose cuttings, then driven an additional 12 inches with blows of a 140-pound hammer falling 30 inches. The number of hammer blows required to drive the sampler through the two final six inch increments was recorded as the penetration resistance (SPT N) value. The N-value, when properly interpreted by qualified professional staff, is an index of the soil strength and foundation support capability.

Subsurface Water Level Determination

Subsurface water levels in the borings were measured during the onsite exploration by measuring depths from the existing grade to the current water level using a tape.

SUMMARY OF LABORATORY TESTING PROCEDURES

Examination of Recovered Soil Samples

Soil and field records were reviewed in the laboratory by the geotechnical professional. Soils were classified in general accordance with the visual-manual method described in ASTM D 2488, “*Standard Practice for Description and Identification of Soils (Visual-Manual Method)*”. Representative soil samples were selected for classification testing to provide grain size and plasticity data to allow classification of the samples in general accordance with the Unified Soil Classification System method described in ASTM D 2487, “*Standard Practice for Classification of Soils for Engineering Purposes*”. The geotechnical professional also prepared the final boring and sounding records enclosed with this report.

Moisture Content Testing of Soil Samples by Oven Drying

Moisture content was determined in general conformance with the methods outlined in ASTM D 2216, “*Standard Test Method for Laboratory Determination of Water (Moisture) Content of Soil or Rock by Mass.*” This method is limited in scope to Group B, C, or D samples of earth materials which do not contain appreciable amounts of organic material, soluble solids such as salt or reactive solids such as cement. This method is also limited to samples which do not contain contamination.

A representative portion of the soil was divided from the sample using one of the methods described in Section 9 of ASTM D 2216. The split portion was then placed in a drying oven and heated to approximately 110 degrees C overnight or until a constant mass was achieved after repetitive weighing. The moisture content of the soil was then computed as the mass of water removed from the sample by drying, divided by the mass of the sample dry, times 100 percent. No attempt was made to exclude any particular particle size from the portion split from the sample.

Liquid and Plastic Limits Testing

Atterberg limits of the soils was determined generally following the methods described by ASTM D 4318, “*Standard Test Methods for Liquid Limit, Plastic Limit, and Plasticity Index of Soils.*” Albert Atterberg originally defined “limits of consistency” of fine grained soils in terms of their relative ease of deformation at various moisture contents. In current engineering usage, the *liquid limit* of a soil is defined as the moisture content, in percent, marking the upper limit of viscous flow and the boundary with a semi-liquid state. The *plastic limit* defines the lower limit of plastic behavior, above which a soil behaves plastically below which it retains its shape upon drying. The *plasticity index* (PI) is the range of water content over which a soil behaves plastically. Numerically, the PI is the difference between liquid limit and plastic limit values.

Representative portions of fine grained Group A, B, C, or D samples were prepared using the wet method described in Section 10.1 of ASTM D 4318. The liquid limit of each sample was determined using the multipoint method (Method A) described in Section 11, or the one-point method (Method B) described in Section 13. The liquid limit is by

definition the moisture content where 25 drops of a hand operated liquid limit device are required to close a standard width groove cut in a soil sample placed in the device.

Multi-Point Method

After each test, the moisture content of the sample was adjusted and the sample replaced in the device. The test was repeated to provide a minimum of three widely spaced combinations of N versus moisture content. When plotted on semi-log paper, the liquid limit moisture content was determined by straight line interpolation between the data points at N equals 25 blows.

One-Point Method

The procedure for the one-point method is the same as the multi-point method except that the number of blows required to close the groove is 20 to 30. If less than 20 or more than 30 blows are required, the water content of the soil is adjusted and the procedure is repeated. The liquid limit is determined in accordance with Section 14.

The plastic limit was determined using the procedure described in Sections 15 through 17 of ASTM D 4318. A selected portion of the soil used in the liquid limit test was kneaded and rolled by hand until it could no longer be rolled to a 3.2 mm thread on a glass plate. This procedure was repeated until at least 6 grams of material was accumulated, at which point the moisture content was determined using the methods described in ASTM D 2216.

Grain Size Analysis of Samples



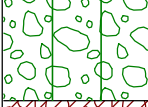
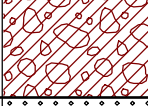
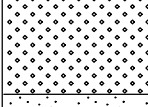
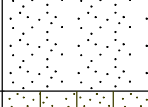
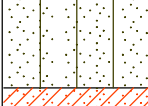
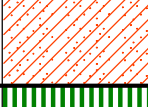
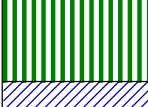
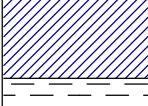
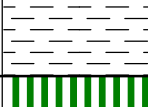
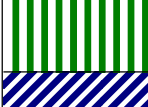
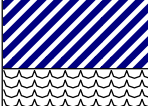


The distribution of particle sizes greater than 75 μ m was determined in general accordance with the procedures described by ASTM D 421, "*Standard Practice for Dry Preparation of Soil Samples for Particle-Size Analysis and Determination of Soil Constants*", and D 422, "*Standard Test Method for Particle Size Analysis of Soils*," except that the hydrometer portion of the test standard was not utilized. During preparation samples were divided into two portions. The material coarser than the No. 30 U.S. sieve size fraction was dry sieved through a nest of standard sieves as described in Article 6. Material passing the No. 30 sieve was independently passed through a nest of sieves down to the No. 200 size.

Percent Fines Determination of Samples

A selected specimen of soils was washed over a No. 200 sieve after being thoroughly mixed and dried. This test was conducted in general accordance with ASTM D 1140, "*Standard Test Method for Amount of Material Finer Than the No. 200 Sieve*." Method A, using water to wash the sample through the sieve without soaking the sample for a prescribed period of time, was used and the percentage by weight of material washing through the sieve was deemed the "percent fines" or percent clay and silt fraction.

SOIL CLASSIFICATION CHART

NOTE: DUAL SYMBOLS ARE USED TO INDICATE BORDERLINE SOIL CLASSIFICATIONS

MAJOR DIVISIONS			SYMBOLS		TYPICAL DESCRIPTIONS
			GRAPH	LETTER	
COARSE GRAINED SOILS	GRAVEL AND GRAVELLY SOILS	CLEAN GRAVELS (LITTLE OR NO FINES)		GW	WELL-GRADED GRAVELS, GRAVEL - SAND MIXTURES, LITTLE OR NO FINES
		GRAVELS WITH FINES (APPRECIABLE AMOUNT OF FINES)		GP	POORLY-GRADED GRAVELS, GRAVEL - SAND MIXTURES, LITTLE OR NO FINES
		GRAVELS WITH FINES (APPRECIABLE AMOUNT OF FINES)		GM	SILTY GRAVELS, GRAVEL - SAND - SILT MIXTURES
		GRAVELS WITH FINES (APPRECIABLE AMOUNT OF FINES)		GC	CLAYEY GRAVELS, GRAVEL - SAND - CLAY MIXTURES
	SAND AND SANDY SOILS	CLEAN SANDS (LITTLE OR NO FINES)		SW	WELL-GRADED SANDS, GRAVELLY SANDS, LITTLE OR NO FINES
		CLEAN SANDS (LITTLE OR NO FINES)		SP	POORLY-GRADED SANDS, GRAVELLY SAND, LITTLE OR NO FINES
		SANDS WITH FINES (APPRECIABLE AMOUNT OF FINES)		SM	SILTY SANDS, SAND - SILT MIXTURES
		SANDS WITH FINES (APPRECIABLE AMOUNT OF FINES)		SC	CLAYEY SANDS, SAND - CLAY MIXTURES
FINE GRAINED SOILS	SILTS AND CLAYS	LIQUID LIMIT LESS THAN 50		ML	INORGANIC SILTS AND VERY FINE SANDS, ROCK FLOUR, SILTY OR CLAYEY FINE SANDS OR CLAYEY SILTS WITH SLIGHT PLASTICITY
				CL	INORGANIC CLAYS OF LOW TO MEDIUM PLASTICITY, GRAVELLY CLAYS, SANDY CLAYS, SILTY CLAYS, LEAN CLAYS
				OL	ORGANIC SILTS AND ORGANIC SILTY CLAYS OF LOW PLASTICITY
	SILTS AND CLAYS	LIQUID LIMIT GREATER THAN 50		MH	INORGANIC SILTS, MICACEOUS OR DIATOMACEOUS FINE SAND OR SILTY SOILS
				CH	INORGANIC CLAYS OF HIGH PLASTICITY
				OH	ORGANIC CLAYS OF MEDIUM TO HIGH PLASTICITY, ORGANIC SILTS
HIGHLY ORGANIC SOILS				PT	PEAT, HUMUS, SWAMP SOILS WITH HIGH ORGANIC CONTENTS



PROJECT:		Crystal Lakes Myrtle Beach, South Carolina S&ME Project No. 1633-13-127			BORING LOG B-1									
DATE DRILLED: 5/1/13		ELEVATION:		NOTES:										
DRILL RIG: CME 45-B		BORING DEPTH: 20.0 ft												
DRILLER: Gerald		WATER LEVEL: 0' 24 hr												
HAMMER TYPE: Automatic		LOGGED BY: Chris Brown												
SAMPLING METHOD: Split spoon				NORTHING:		EASTING:								
DRILLING METHOD: Mud Rotary														
DEPTH (feet)	GRAPHIC LOG	MATERIAL DESCRIPTION	WATER LEVEL	ELEVATION (feet)	SAMPLE NO.	SAMPLE TYPE	BLOW COUNT / CORE DATA			STANDARD PENETRATION TEST DATA (blows/ft) /REMARKS				N VALUE
							1st 6in / RUN #	2nd 6in / REC	3rd 6in / ROD	10	20	30	6080	
		TOPSOIL - Approximately 3 inches thick.												
5		SILTY SAND (SM) - Mostly fine to medium sand, some low to medium plasticity fines, dark brown, wet to saturated, medium dense to loose.			1	3	3	8	8					16
					2	3	7	8						15
					3	5	4	4						8
10		POORLY GRADED SAND (SP) - Mostly fine to medium sand, trace of low to medium plasticity fines, gray, saturated, very loose to loose.			4	3	2	2						4
					5	2	3	3						6
15														
20		Boring terminated at 20 ft			6	3	3	3						6

S&ME BORING LOG - SPT LOGS.GPJ S&ME.GDT 5/16/13

NOTES:

1. THIS LOG IS ONLY A PORTION OF A REPORT PREPARED FOR THE NAMED PROJECT AND MUST ONLY BE USED TOGETHER WITH THAT REPORT.
2. BORING, SAMPLING AND PENETRATION TEST DATA IN GENERAL ACCORDANCE WITH ASTM D-1586.
3. STRATIFICATION AND GROUNDWATER DEPTHS ARE NOT EXACT.
4. WATER LEVEL IS AT TIME OF EXPLORATION AND WILL VARY.




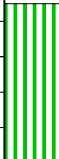



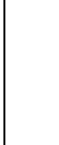
PROJECT:		Crystal Lakes Myrtle Beach, South Carolina S&ME Project No. 1633-13-127			BORING LOG B-2									
DATE DRILLED: 5/1/13		ELEVATION:		NOTES:										
DRILL RIG: CME 45-B		BORING DEPTH: 20.0 ft												
DRILLER: Gerald		WATER LEVEL: 0' 24 hr												
HAMMER TYPE: Automatic		LOGGED BY: Chris Brown												
SAMPLING METHOD: Split spoon				NORTHING:		EASTING:								
DRILLING METHOD: Mud Rotary														
DEPTH (feet)	GRAPHIC LOG	MATERIAL DESCRIPTION	WATER LEVEL	ELEVATION (feet)	SAMPLE NO.	SAMPLE TYPE	BLOW COUNT / CORE DATA			STANDARD PENETRATION TEST DATA (blows/ft) /REMARKS				N VALUE
							1st 6in / RUN #	2nd 6in / REC	3rd 6in / ROD	10	20	30	6080	
		TOPSOIL - Approximately 3 inches thick.												
5		POORLY GRADED SAND (SP) - Mostly fine to coarse sand, trace of low to medium plasticity fines, brown, tan, and gray, wet to saturated, very loose to loose. ----- Finger size roots from 0 to 2.5 feet.			1	2	2	3						5
					2	3	3	3						6
					3	1	2	2						4
					4	2	2	2						4
					5	3	3	2						5
					6	2	3	2						5
		Boring terminated at 20 ft												

S&ME BORING LOG - SPT LOGS.GPJ S&ME.GDT 5/16/13

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PROJECT:		Crystal Lakes Myrtle Beach, South Carolina S&ME Project No. 1633-13-127			BORING LOG B-3									
DATE DRILLED: 5/1/13		ELEVATION:		NOTES:										
DRILL RIG: CME 45-B		BORING DEPTH: 30.0 ft												
DRILLER: Gerald		WATER LEVEL: 3.5' 24 hr												
HAMMER TYPE: Automatic		LOGGED BY: Chris Brown												
SAMPLING METHOD: Split spoon				NORTHING:		EASTING:								
DRILLING METHOD: Mud Rotary														
DEPTH (feet)	GRAPHIC LOG	MATERIAL DESCRIPTION	WATER LEVEL	ELEVATION (feet)	SAMPLE NO.	SAMPLE TYPE	BLOW COUNT / CORE DATA			STANDARD PENETRATION TEST DATA (blows/ft) /REMARKS				N VALUE
							1st 6in / RUN #	2nd 6in / REC	3rd 6in / ROD	10	20	30	6080	
5		POORLY GRADED SAND (SP) - Mostly fine to medium sand, trace of low to medium plasticity fines, brown, moist to wet, very loose to medium dense.	▼		1	3	3	4	4					8
10		ELASTIC SILT WITH SAND (ML) - Mostly medium to low plastic fines, few fine sands, gray, saturated, very soft.			2	9	10	7						17
15		POORLY GRADED SAND (SP) - Mostly fine to medium sand, trace of low to medium plasticity fines, gray, tan and brown, saturated, loose to medium dense.			3	3	1	2						3
20					4	1	1	0						1
25					5	4	4	4						8
30					6	4	3	2						5
					7	5	5	5						10
					8	5	6	6						12
		Boring terminated at 30 ft												

S&ME BORING LOG - SPT LOGS.GPJ S&ME.GDT 5/16/13

NOTES:

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3. STRATIFICATION AND GROUNDWATER DEPTHS ARE NOT EXACT.
4. WATER LEVEL IS AT TIME OF EXPLORATION AND WILL VARY.



PROJECT:		Crystal Lakes Myrtle Beach, South Carolina S&ME Project No. 1633-13-127		BORING LOG B-4											
DATE DRILLED: 5/1/13		ELEVATION:		NOTES:											
DRILL RIG: CME 45-B		BORING DEPTH: 30.0 ft													
DRILLER: Gerald		WATER LEVEL: 10' 24 hr													
HAMMER TYPE: Automatic		LOGGED BY: Chris Brown													
SAMPLING METHOD: Split spoon				NORTHING:		EASTING:									
DRILLING METHOD: Mud Rotary															
DEPTH (feet)	GRAPHIC LOG	MATERIAL DESCRIPTION	WATER LEVEL	ELEVATION (feet)	SAMPLE NO.	SAMPLE TYPE	BLOW COUNT / CORE DATA			STANDARD PENETRATION TEST DATA (blows/ft) /REMARKS				N VALUE	
							1st 6in / RUN #	2nd 6in / REC	3rd 6in / ROD	10	20	30	6080		
		TOPSOIL - Approximately 3 inches thick.													
5		POORLY GRADED SAND (SP) - Mostly fine to medium sand, trace of low to medium plasticity fines, tan and brown, moist to wet, very loose to loose.			1	4	4	5							9
					2	4	3	3							6
					3	1	2	2							4
10			▼		4	1	2	2							4
15		SILTY SAND (SM) - Mostly fine to medium sand, some low to medium plasticity fines, dark brown, wet to saturated, loose.			5	4	4	4							8
20					6	3	4	3							7
25		POORLY GRADED SAND (SP) - Mostly fine to medium sand, trace of low to medium plasticity fines, gray, saturated, loose to medium dense.			7	3	4	5							9
30		Boring terminated at 30 ft			8	6	6	7							13

S&ME BORING LOG - SPT LOGS.GPJ S&ME.GDT 5/16/13

NOTES:

1. THIS LOG IS ONLY A PORTION OF A REPORT PREPARED FOR THE NAMED PROJECT AND MUST ONLY BE USED TOGETHER WITH THAT REPORT.
2. BORING, SAMPLING AND PENETRATION TEST DATA IN GENERAL ACCORDANCE WITH ASTM D-1586.
3. STRATIFICATION AND GROUNDWATER DEPTHS ARE NOT EXACT.
4. WATER LEVEL IS AT TIME OF EXPLORATION AND WILL VARY.

